EXPERIMENTAL ACTIVITIES FOR GSI-191

Department of Nuclear Engineering, Texas A&M University

INTRODUCTION

Generic Safety Issue 191 (GSI-191), “Assessment of Debris Accumulation on PWR Sump Performance”, can be categorized into the head loss through a debris bed on the strainer (the upstream effect) and the debris penetration through the strainer (the downstream effect). Texas A&M University (TAMU) has constructed test facilities and been performing experimental activities to understand and resolve the both effects. Also, TAMU has developed techniques to characterize the debris size distribution, from nanometers to macro size (millimeters). TAMU is modifying the facilities to conduct chemical experiments to analyze the effect of chemicals on head loss and debris penetration.

RESEARCH OBJECTIVES

- Head loss and Debris Bypass through the fibrous bed generated on strainers
- Effects of fluid temperature and approach velocity on head loss and debris bypass
- Effects of additional chemicals and particles on head loss and debris bypass
- Water chemistry effects on debris Bypass
- Characterization of debris size distribution
- Thermal-hydraulic calculation to provide the containment and primary system condition using RELAP5-3D and MELCOR.

EXPERIMENTAL FACILITIES

- High Temperature Vertical Loop - 185 °F (85 °C), 6” ID Test Section
- High Temperature Horizontal Loop - 185 °F (85 °C), 4” ID Test Section
- Low Temperature Horizontal Loop - 113 °F (45 °C), 4” ID Test Section
- Debris Size Characterization Systems - nanometers to millimeters
- Chemical Analysis Systems - XRD, XRD, ICP-MS, XPS, and NMR

PUBLICATIONS

High Temperature Vertical Loop for Measurement of Head Loss and Debris Bypass

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CAPABILITIES

- Approach Velocity: 0.005 ~ 0.5 ft/s
- Temperature: 185 °F (85 °C)
- Different Strainer Types Applicable
- Dynamic and Integral Debris Sampling
- Facility Components Chemical-resistant

PUBLICATIONS

Head Loss & Chemical Effects Experiment Facility

CAPABILITIES

- Includes all the capabilities of the high temperature vertical loop
- Measurements of head loss through fibrous and particulate debris beds
- Chemically-induced head loss evaluation
- High accuracy pressure drop instrumentations for different pressure ranges
- Corrosion tanks can be connected to the horizontal loop (see next slide)
High Temperature Horizontal Loop for Measurement of Head Loss and Debris Bypass

CAPABILITIES

• Approach Velocity: 0.005 ~ 0.5 ft/s
• Temperature: 185 °F (85 °C)
• Different Strainer Types Applicable
• Dynamic and Integral Debris Sampling
• Facility Components Chemical-resistant

PUBLICATIONS

• Saya Lee, Yassin A. Hassan, Rodolfo Vaghetto, Suhaeb Abdulsattar, Matthew Kappes, "WATER CHEMISTRY SENSITIVITY ON FIBROUS DEBRIS BYPASS THROUGH A CONTAINMENT SUMP STRAINER," Proceedings of the 2014 22nd International Conference on Nuclear Engineering, ICONE22, July 7-11, 2014, Prague, Czech Republic

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Low Temperature Horizontal Loop for Measurement of Head Loss and Debris Bypass

**CAPABILITIES**
- Approach Velocity: 0.005 ~ 0.1 ft/s
- Temperature: 113 °F (45 °C)
- Strainer Exchangeable
- Dynamic Debris Sampling
- Chemical Resistance

**PUBLICATIONS**
- Saya Lee, Suhaeb Abdulsattar, Rodolfo Vaghetto, Yassin A. Hassan, “Experimental Study Of Fibrous Debris Head Loss Through Sump Strainer,” Advances in Thermal Hydraulics (ATH '12), November 11-15 2012, San Diego, CA.
Debris Sampling and Size Characterization

DYNAMIC SAMPLING
The sampling port installed downstream of the strainer allows dynamic sampling at the same flow speed without disturbing the flow, which is known as isokinetic sampling.

Isokinetic Sampling Probe

SIZE CHARACTERIZATION

Upstream debris size distribution

Downstream debris size distribution
Submicron Size Characterization Capabilities

SEM

- Magnifications up to 1,000,000x
- Guaranteed resolution: 1 nm.

NUKON debris

Tin particles

Electronic Sensing Zone (ESZ) technique

Using ESZ
Nano-Size Characterization Capabilities

NANOSIGHT

- Size resolution: 2nm
- Range: 2 – 1000 nm

Particle size distribution from NanoSight software
Chemical Precipitate Characterization

**Analysis**
- ICP-OES or ICP-MS (filtered and total)
- Particle size distribution
- XRD
- NMR (B, Al, Si)
- TEM
- XPS
- Viscosity and Turbidity

**XPS Spectrum**

**ICP-MS**

**Raman/FTIR**

**NMR**

**TEM**

Magnification range: 21x - 410x
Point resolution: 0.27 nm

**Viscosity**

The accuracies of MCR 300 Rheometer are:
- Viscosity: ± 0.5%
- Temperature: ± 0.1 °C

TAMU performed viscosity measurement of buffered borated water with trisodium phosphate or NaOH. The Method was validated by comparing the measured viscosity of deionized (DI) water to the data given by NIST.

**Viscosity of DI water**

![Graph showing viscosity of DI water]

**Buffered/Borated**

![Graph showing viscosity of buffered borated water]
TAMU has developed standardized models of the primary system and reactor containment with system codes largely used in analysis of LWR transients. RELAP5-3D models of different US PWRs have been prepared and currently used to perform thermal-hydraulic simulations to support the GSI-191. MELCOR models of reactor containments are being used to perform the simulations of the containment response during LOCA. RELAP5-3D and MELCOR have been linked to perform simultaneous simulations of the primary system and containment response during LOCA scenarios under different plant conditions. Other computational capabilities include Computational fluid Dynamics CFD (Star-CCM+, Neptune, CFX, Fluent), sub-channel codes (COBRA-TF) and other system codes (GOTHIC).

The models developed have been used for:
- Predict the system response during LOCA scenarios under hypothetical full or partial core blockage at the bottom of the core;
- Perform sensitivity analysis of the containment response under different plant configurations including:
  - ECCS pumps availability
  - Containment engineered features availability
  - RWST and CCW temperatures
- Estimate the sump pool temperature profiles used for experimental analysis
- Estimate specific thermal-hydraulic parameters (sump switchover time, sump pool temperature, ECCS flow rates, etc.) as a function of:
  - Break size
  - Break location
  - Other plant conditions
- Support the PRA with specific accident scenarios
RELAP5-3D MULTI-DIMENSIONAL MODEL

A realistic representation of the vessel internals and reactor core has been achieved using the multi-dimensional capabilities of RELAP5-3D. The model simulated the core with 193 fuel assemblies with cross-flow using Cartesian components, including the capability of defining a realistic radial power profile.

A 3D model of the reactor vessel and core has been developed and used to perform simulations of LOCA transients under different hypothetical core blockages scenarios. 3D Visualization tools were developed to perform 3D animations of thermal-hydraulic parameters of interest, and visualize the flow patterns inside the core.

Applications of Computational Fluid Dynamics (CFD)

Department of Nuclear Engineering, Texas A&M University

INTRODUCTION

In the last decade, the Texas A&M University has actively performed the CFD calculations about the nuclear engineering problems. The nuclear engineering problems considered were:

• Two-phase flow (subcooled flow boiling, pool boiling, isothermal two-phase)
• Air-ingress accident in VHTR, Inlet-plenum mixing in VHTR
• Reactor Cavity Cooling System (RCCS)
• Flow in a pebble bed, Flow in a rod bundle
• Debris sedimentation (GSI-191), etc.

CFD CAPABILITIES

Solvers Available

• Commercial CFD codes: ANSYS FLUENT, ANSYS CFX, STAR-CCM+
• Open source CFD codes: OpenFOAM, Code_Saturne, Hydra
• In-house code: Lattice Boltzmann method (LBM) code

CPU Resources

• HPC system- Number of Processing Cores: 3168 (at 2.8 GHz)

APPLICATIONS

Flow in the Lower Plenum of VHTR

Air-Ingress Accident

Reactor Cavity Cooling System (RCCS)
EPRI CFD Round Robin Benchmark for PWR Fuel Rod Assembly

Department of Nuclear Engineering, Texas A&M University

INTRODUCTION

- In-core crudding risk assessment requires local heat transfer information predicted by the computational fluid dynamics (CFD) in a rod bundle.
- The thorough CFD validation should precede the CFD prediction of the local heat transfer.
- Various CFD methodologies can be effectively compared through the round-robin benchmark.
- TAMU has organized and participated in the round robin benchmark against the NESTOR experiment since 2011.
- Ten organizations participated in the Round Robin.

OBJECTIVES

- Benchmark CFD codes to high fidelity experimental data for a rod bundle flow
- Develop the Best Practices Document for CFD users that can be applied to in-core crudding risk (CILC, CIPS, etc.) assessments and future assembly and core designs

NESTOR EXPERIMENT

Phase I (Simple Support Grid)

- Grid span pressure loss (Simple support grid)
- Mean axial velocity (Simple support grid)

Phase II (Mixing vane grid)

- Grid span pressure loss (Mixing vane grid)
- Rod surface temperature (Mixing vane grid)

STRUCTURE OF ROUND ROBIN

Phase I (Simple Support Grid)

- Selected Test Cases
- Run #1
- Run #2
- Run #3
- Run #4
- Run #5
- Run #6
- Run #7
- Run #8
- Run #9
- Run #10
- Run #11

Phase II (Mixing vane grid)

- Selected Test Cases
- Run #1
- Run #2
- Run #3
- Run #4
- Run #5
- Run #6
- Run #7
- Run #8
- Run #9
- Run #10
- Run #11

PUBLICATION

**INTRODUCTION**

- The **Lattice Boltzmann Method (LBM)** is a kinetic approach to solving the fluid field as an alternative to Navier-Stokes equation.
- The LBM has some noted features like simplicity, computational efficiency, parallelism, algebraic operation and particle base scheme that distinguishes it from the other conventional CFD methods.
- The in-house LBM code was developed and has been applied to several engineering problems.

**CAPABILITIES**

**Governing Equations**
- Flow Equation
  - Lattice models: D2Q9, D3Q19, and D3Q27
  - Collision models: SRT, TRT, and MRT
  - Energy Equation
  - D2Q5, D2Q9, D3Q7, D3Q15 thermal LBEs
  - Hybrid models (Finite-difference Eq.)
  - Two-phase flow Equation
  - Cahn-Hillard Equation (D2Q9, D3Q19)

**Turbulence Models**
- LES SGS models
  - Smagorinsky model
  - WALE model
  - Vanre model (w dynamic model)

**Boundary Methods**
- Mesoscopic boundary method
  - Bounce-back scheme (original/modified)
  - Boudou et al. scheme
  - Yu et al. scheme
  - Multi-reflection scheme

- Immersed Boundary Method (IBM)
  - Sharp interface scheme
  - Linear interface extrapolation
  - Bi-linear interpolation
  - Implicit/explicit methods
  - 2, 3, 4, 5, and 6-point discrete delta functions

**Applications**
- Fluid-structure interaction
  - Inline oscillation
  - Crossflow oscillation
  - Flow-induced vibration
  - 1 DOF
  - 2 DOF
- Particle-fluid flow
  - 2D cylinder particle sedimentation
  - 1, 2, and 504 particles
  - 3D spherical particle sedimentation
  - 2, 7, 26, and 2048 particles
  - Oblate spheroidal particle sedimentation
  - 3D particle in a circular pipe flow
  - Particle sedimentation with heat transfer
- (Liquid-vapor) two-phase flow
  - Static bubble (2D/3D)
  - Single bubble rising in a channel

**APPLICATIONS** – Large Eddy Simulation (LES)

- Flow in a Rod Bundle
- Cross-flow over a Rod Bundle
- Flow in a Pebble Bed

**PUBLICATIONS (selected)**

INTRODUCTION

- Coupled with the immersed boundary method (IBM), the lattice Boltzmann method (LBM) has been applied to fluid-solid interaction problems, such as particle sedimentation, particulate flows, and fluid-structure interaction.
- The direct numerical simulation based on the two-way coupling between solid and fluid was performed.

PARTICLE SEDIMENTATION

FLUID-STRUCTURE INTERACTION

PUBLICATIONS (selected)